

Semnan University Faculty of Mechanical Engineering



دانشکده مهندسی مکانیک

درس دینآمیک

# **ENGINEERING MECHANICS DYNAMICS**

MERIAM, KRAIGE & BOLTON 9<sup>TH</sup> EDITION

Chapter 5: Plane Kinetics of Rigid Bodies

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## CHAPTER 6

# Plane Kinetics of Rigid Bodies

#### CHAPTER OUTLINE

6/1 Introduction

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- 6/2 General Equations of Motion
- 6/3 Translation
- 6/4 Fixed-Axis Rotation
- 6/5 General Plane Motion

#### SECTION B Work and Energy

- 6/6 Work-Energy Relations
- 6/7 Acceleration from Work-Energy; Virtual Work

#### SECTION C Impulse and Momentum

- 6/8 Impulse-Momentum Equations
- 6/9 Chapter Review



The principles of this chapter must be applied during the design of the massive blades of large wind turbines.



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### 6/1 Introduction

- The kinetics of rigid bodies treats the relationships between the external forces acting on a body and the corresponding translational and rotational motions of the body
- For our purpose, a body which can be approximated as a thin slab with its motion confined to the plane of the slab will be considered to be in plane motion.
  - ✓ Section A: forces and moments to instantaneous linear and angular accelerations relations
  - ✓ Section B: method of work and energy
  - ✓ Section C: methods of impulse and momentum

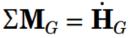


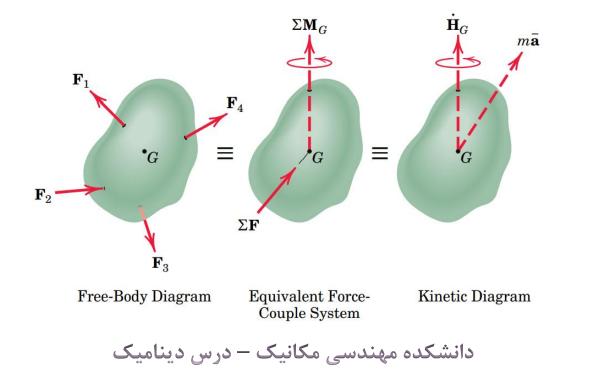
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### SECTION A Force, Mass, and Acceleration

<sup>6/2</sup> General Equations of Motion

- $\Box \text{ The force equation:} \qquad \Sigma \mathbf{F} = m \overline{\mathbf{a}}$
- □ The moment equation taken about the mass center:



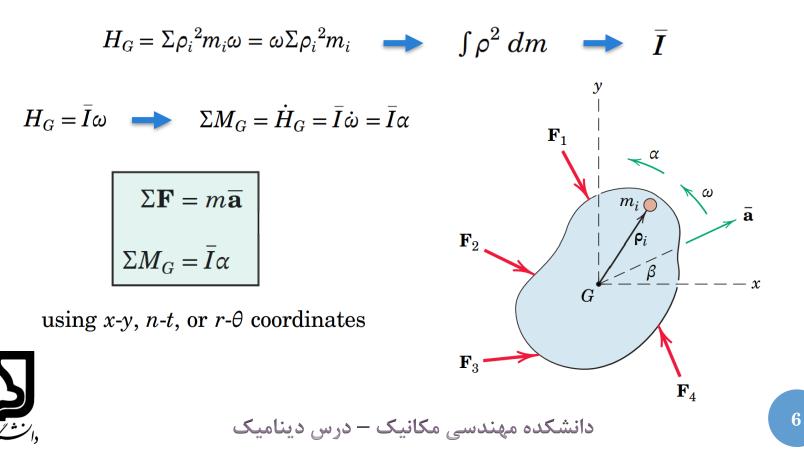




#### **Plane-Motion Equations**

A rigid body moving with plane motion in the x-y plane

✓ The mass moment of inertia:



#### **Alternative Derivation**

\* By referring directly to the forces which act on the representative particle of mass  $m_i$ 

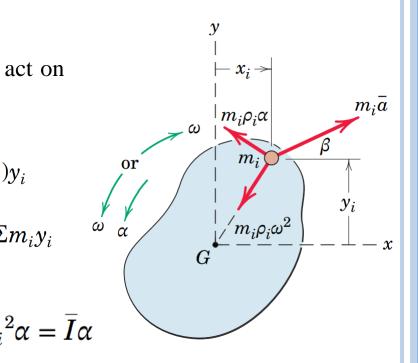
$$M_{G_i} = m_i \rho_i^2 \alpha + (m_i \overline{a} \sin \beta) x_i - (m_i \overline{a} \cos \beta) y_i$$

$$\Sigma M_G = \Sigma m_i \rho_i^2 \alpha + \overline{a} \sin \beta \Sigma m_i x_i - \overline{a} \cos \beta \Sigma m_i y_i$$

$$\Sigma m_i x_i = m \overline{x} = 0$$
  

$$\Sigma m_i y_i = m \overline{y} = 0$$

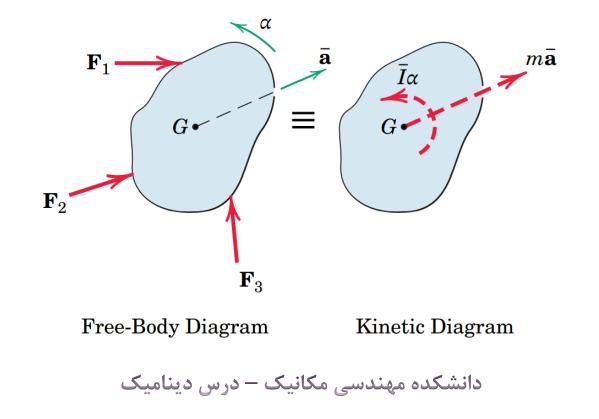
$$\Sigma M_G = \Sigma m_i \rho_i$$





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- ✓ The free-body diagram discloses the forces and moments appearing on the lefthand side of equations of motion.
- ✓ The kinetic diagram discloses the resulting dynamic response in terms of the translational term and the rotational term which appear on the right-hand side of equations of motion.

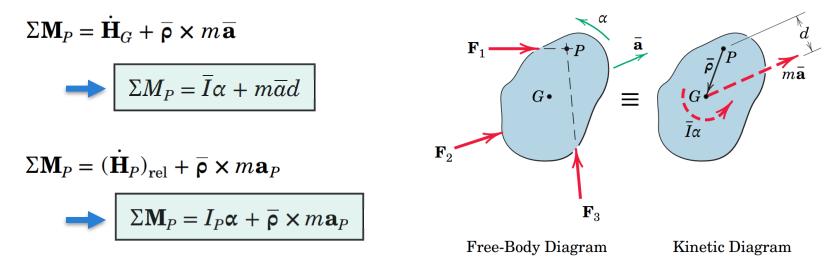




### <sup>6/2</sup> General Equations of Motion

### **Alternative Moment Equations**

General equation for moments about an arbitrary point P



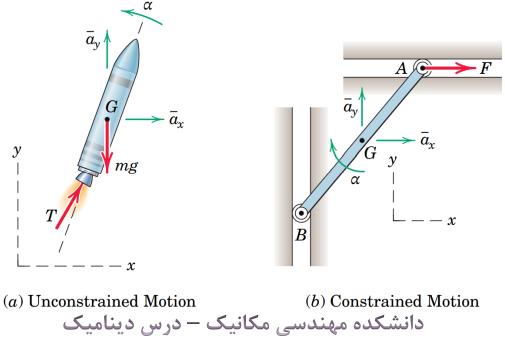
✓ When point P becomes a point O fixed in an inertial reference system

$$\Rightarrow \quad \Sigma M_O = I_O \alpha$$



#### **Unconstrained and Constrained Motion**

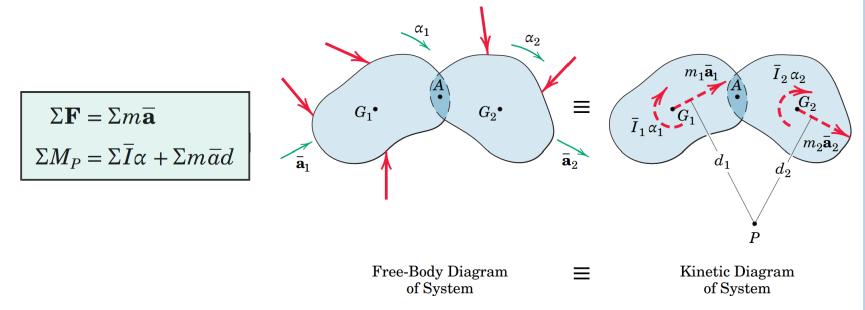
- The motion of a rigid body may be unconstrained or constrained.
- \* The two components  $a_x$  and  $a_y$  of the mass center acceleration and the angular acceleration  $\alpha$  may be determined independently or not.
- In general, dynamics problems which involve physical constraints to motion require a kinematic analysis relating linear to angular acceleration before the force and moment equations of motion can be solved.





#### Systems of Interconnected Bodies

✓ In problems dealing with two or more connected rigid bodies whose motions are related kinematically, it is convenient to analyze the bodies as an entire system.



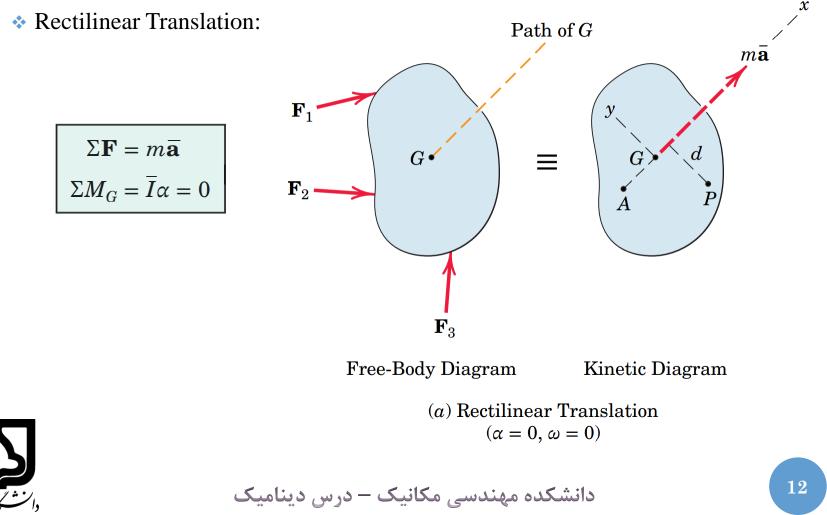
✓ If there are more than three remaining unknowns, the E.O.M. is not sufficient to solve the problem.



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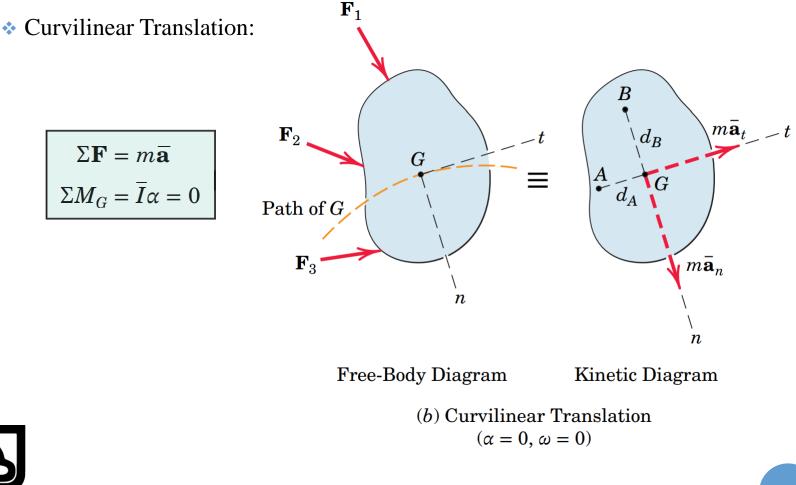
### <sup>6/3</sup> Translation

□ There is no angular motion of the translating body, so that both  $\omega$  and  $\alpha$  are zero.



### <sup>6/3</sup> Translation

There is no angular motion of the translating body, so that both  $\omega$  and  $\alpha$  are zero.



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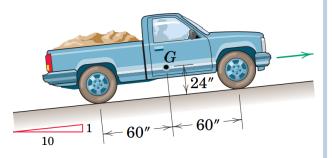
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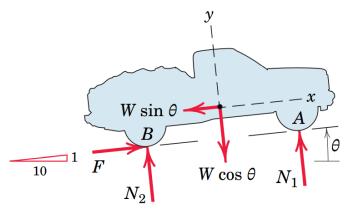
The pickup truck weighs 3220 lb and reaches a speed of 30 mi/hr from rest in a distance of 200 ft up the 10-percent incline with constant acceleration. Calculate the normal force under each pair of wheels and the friction force under the rear driving wheels. The effective coefficient of friction between the tires and the road is known to be at least 0.80.

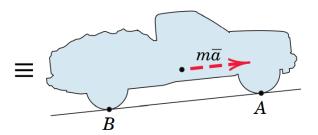
$$m\overline{a} = \frac{3220}{32.2}(4.84) = 484$$
 lb

$$\begin{split} [\Sigma F_x &= m \bar{a}_x] & F - 320 = 484 & F = 804 \ \text{lb} \\ [\Sigma F_y &= m \bar{a}_y = 0] & N_1 + N_2 - 3200 = 0 \\ [\Sigma M_G &= \bar{I}\alpha = 0] & 60N_1 + 804(24) - N_2(60) = 0 \end{split}$$

$$\implies N_1 = 1441 \text{ lb} \qquad N_2 = 1763 \text{ lb}$$

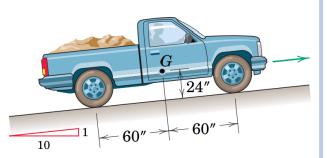




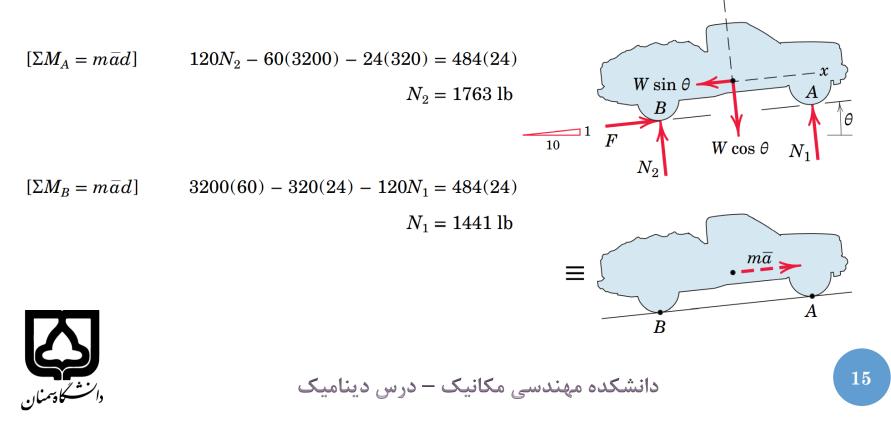




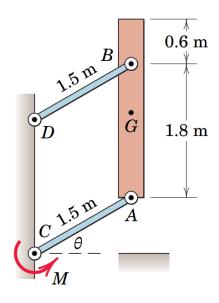
The pickup truck weighs 3220 lb and reaches a speed of 30 mi/hr from rest in a distance of 200 ft up the 10-percent incline with constant acceleration. Calculate the normal force under each pair of wheels and the friction force under the rear driving wheels. The effective coefficient of friction between the tires and the road is known to be at least 0.80.

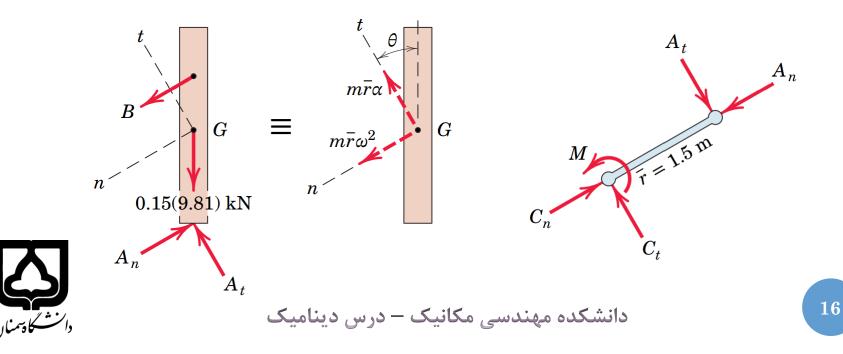


#### **Alternative Solution**



The vertical bar *AB* has a mass of 150 kg with center of mass *G* midway between the ends. The bar is elevated from rest at  $\theta = 0$  by means of the parallel links of negligible mass, with a constant couple  $M = 5 \text{ kN} \cdot \text{m}$  applied to the lower link at *C*. Determine the angular acceleration  $\alpha$  of the links as a function of  $\theta$  and find the force *B* in the link *DB* at the instant when  $\theta = 30^{\circ}$ .





 $\equiv$ 

n

 $A_t$ 

r = 1.5 m

 $C_t$ 

t

 $m\overline{r}\alpha$ 

 $m\bar{r}\omega^2$ 

θ

G

 $A_n$ 

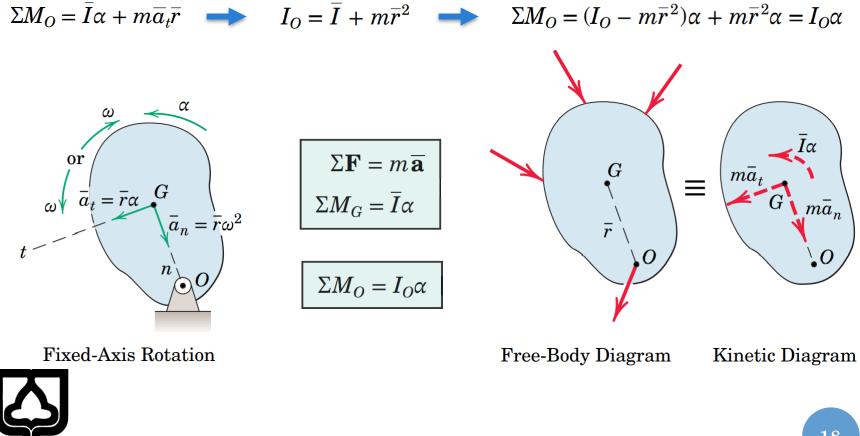
$$\begin{split} A_t &= M/\overline{AC} = 5/1.5 = 3.33 \text{ kN} \\ [\Sigma F_t &= m\overline{a}_t] & 3.33 - 0.15(9.81) \cos \theta = 0.15(1.5\alpha) \\ &\alpha &= 14.81 - 6.54 \cos \theta \text{ rad/s}^2 \\ [\omega \ d\omega &= \alpha \ d\theta] & \int_0^{\omega} \omega \ d\omega &= \int_0^{\theta} (14.81 - 6.54 \cos \theta) \ d\theta \\ &\omega^2 &= 29.6\theta - 13.08 \sin \theta \\ & &\omega^2 &= 29.6\theta - 13.08 \sin \theta \\ & & &A_n & A_t \\ & & & & & \\ \mathbf{M} \overline{r} \omega^2 &= 0.15(1.5)(8.97) = 2.02 \text{ kN} \\ &m\overline{r} \alpha &= 0.15(1.5)(9.15) = 2.06 \text{ kN} \\ [\Sigma M_A &= m\overline{a}d] & 1.8 \cos 30^{\circ} B &= 2.02(1.2) \cos 30^{\circ} + 2.06(0.6) \\ & & & & \\ B &= 0.14 \text{ kN} \end{split}$$

B = 2.14 kN



### <sup>6/4</sup> Fixed-Axis Rotation

\* All points in the body describe circles about the rotation axis, and all lines of the body in the plane of motion have the same angular velocity  $\omega$  and angular acceleration  $\alpha$ .



### <sup>6/4</sup> Fixed-Axis Rotation

- Center of Percussion
  - \* We may combine the resultant-force component mat and resultant couple I $\alpha$  by moving mat to a parallel position through point Q on line OG.

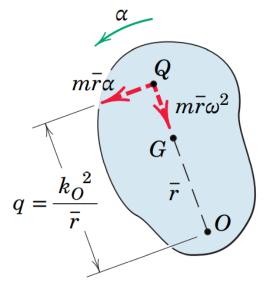
$$m\bar{r}\alpha q = \bar{I}\alpha + m\bar{r}\alpha(\bar{r})$$

 $I_O = k_O^2 m \quad \Longrightarrow \quad q = k_O^2 / \bar{r}$ 

- Point Q is called the center of percussion and has the unique property that the resultant of all forces applied to the body must pass through it.
- It follows that the sum of the moments of all forces about the center of percussion is always zero

 $\Sigma M_Q = 0$ 





The pendulum has a mass of 7.5 kg with center of mass at *G* and has a radius of gyration about the pivot *O* of 295 mm. If the pendulum is released from rest at  $\theta = 0$ , determine the total force supported by the bearing at the instant when  $\theta = 60^{\circ}$ . Friction in the bearing is negligible.

$$\begin{split} [\Sigma M_O = I_O \alpha] & 7.5(9.81)(0.25) \cos \theta = (0.295)^2 (7.5) \alpha \\ \alpha = 28.2 \cos \theta \text{ rad/s}^2 \\ [\omega \, d\omega = \alpha \, d\theta] & \int_0^\omega \omega \, d\omega = \int_0^{\pi/3} 28.2 \cos \theta \, d\theta \end{split}$$

 $\omega^2 = 48.8 \, (rad/s)^2$ 

$$O_n$$

$$O_t$$

7.5(9.81) N

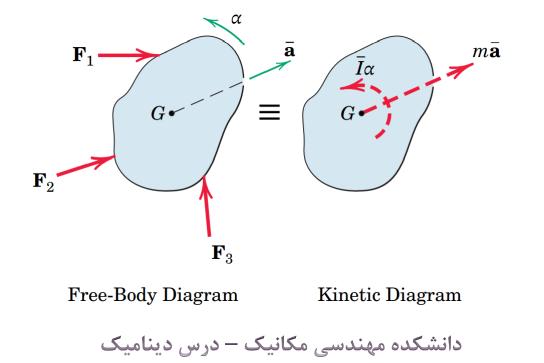


$$\begin{split} [\Sigma F_n = m\bar{r}\omega^2] & O_n - 7.5(9.81) \sin 60^\circ = 7.5(0.25)(48.8) \\ O_n = 155.2 \text{ N} \\ [\Sigma F_t = m\bar{r}\alpha] & -O_t + 7.5(9.81) \cos 60^\circ = 7.5(0.25)(28.2) \cos 60^\circ \\ O_t = 10.37 \text{ N} \\ & \bullet \quad O = \sqrt{(155.2)^2 + (10.37)^2} = 155.6 \text{ N} \\ [q = k_0^2/\bar{r}] & q = \frac{(0.295)^2}{0.250} = 0.348 \text{ m} \\ [\Sigma M_q = 0] & O_t(0.348) - 7.5(9.81)(\cos 60^\circ)(0.348 - 0.250) = 0 \\ O_t = 10.37 \text{ N} \\ \hline O_t = 10.37 \text{ N} \\$$

### <sup>6/5</sup> General Plane Motion

The dynamics of a rigid body in general plane motion combines translation and rotation.

$$\Sigma \mathbf{F} = m \overline{\mathbf{a}}$$
$$\Sigma M_G = \overline{I} \alpha$$





A metal hoop with a radius r = 6 in. is released from rest on the 20° incline. If the coefficients of static and kinetic friction are  $\mu_s = 0.15$  and  $\mu_k = 0.12$ , determine the angular acceleration  $\alpha$  of the hoop and the time *t* for the hoop to move a distance of 10 ft down the incline.

Assume that the hoop rolls without slipping

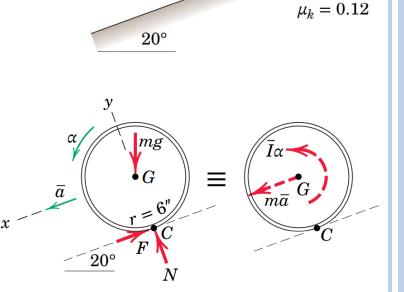
 $\overline{a} = r\alpha$ 

$$\begin{split} [\Sigma F_x &= m \overline{a}_x] & mg \sin 20^\circ - F &= m \overline{a} \\ [\Sigma F_y &= m \overline{a}_y &= 0] & N - mg \cos 20^\circ &= 0 \\ [\Sigma M_G &= \overline{I}\alpha] & Fr &= mr^2 \alpha \end{split}$$

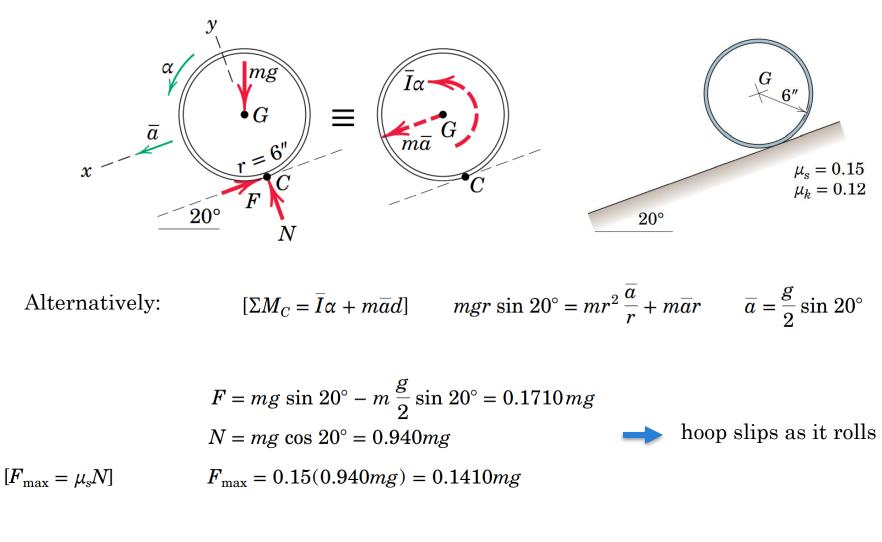
$$\overrightarrow{a} = \frac{g}{2} \sin 20^\circ = \frac{32.2}{2} (0.342) = 5.51 \text{ ft/sec}^2$$



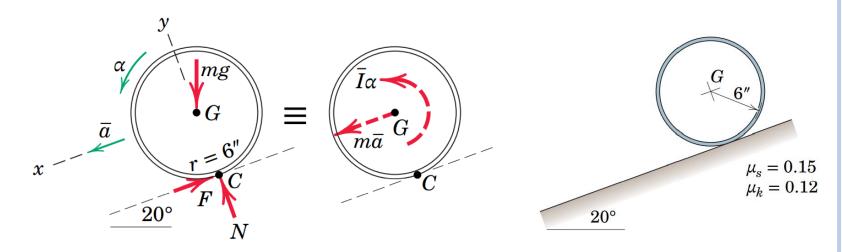
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 $\mu_s=0.15$ 







 $[F = \mu_k N]$ F = 0.12(0.940mg) = 0.1128mg $[\Sigma F_{\rm r} = m\overline{a}_{\rm r}]$  $mg \sin 20^\circ - 0.1128mg = m\overline{a}$  $\overline{a} = 0.229(32.2) = 7.38 \text{ ft/sec}^2$  $[\Sigma M_G = \overline{I}\alpha]$  $0.1128mg(r) = mr^2\alpha$  $\alpha = \frac{0.1128(32.2)}{6/12} = 7.26 \text{ rad/sec}^2$  $[x = \frac{1}{2}at^2]$   $\longrightarrow$   $t = \sqrt{\frac{2x}{a}} = \sqrt{\frac{2(10)}{7.38}} = 1.646 \text{ sec}$ دانشکده مهندسی مکانیک – درس دینامیک



 $d\theta$ 

M

### section в Work and Energy

6/6 Work-Energy Relations

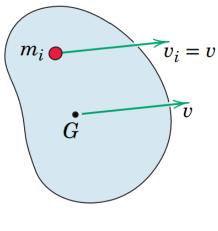
Work of Forces and Couples

$$U = \int \mathbf{F} \cdot d\mathbf{r} \quad \text{or} \quad U = \int (F \cos \alpha) \, ds$$
$$U = \int M \, d\theta$$
$$\overbrace{F}_{B'' b d\theta}_{B'' b d\theta}$$
$$\overbrace{F}_{B'' b d\theta}_{B'' b d\theta} \equiv$$



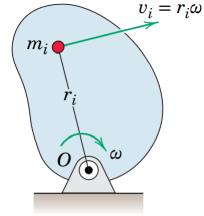
### 6/6 Work-Energy Relations

#### **Kinetic Energy**



(a) Translation

$$T = \frac{1}{2}mv^2$$



(b) Fixed-Axis Rotation

$$T = \frac{1}{2} I_O \omega^2$$

$$P_i \omega - V_i$$

$$w_i + P_i v_i$$

$$\overline{v} + V_i + V_i$$

$$\overline{v} + V_i + V_i$$

$$F = \frac{1}{2}m\overline{v}^2 + \frac{1}{2}\overline{I}\omega^2$$

$$T = \frac{1}{2}I_C\omega^2$$
C: instantaneous center of zero velocity



### 6/6 Work-Energy Relations

### Potential Energy and the Work-Energy Equation

 $\boldsymbol{\ast}$  Gravitational potential energy  $\boldsymbol{V}_g$  and elastic potential energy  $\boldsymbol{V}_e$ 

$$T_1 + U_{1\text{-}2} = T_2$$
 
$$T_1 + V_1 + U_{1\text{-}2}' = T_2 + V_2$$

#### Power

$$P = \frac{dU}{dt} = \frac{\mathbf{F} \cdot d\mathbf{r}}{dt} = \mathbf{F} \cdot \mathbf{v}$$

$$P = \frac{dU}{dt} = \frac{M \, d\theta}{dt} = M\omega$$

$$P = \mathbf{F} \cdot \mathbf{v} + M\omega$$



The wheel rolls up the incline on its hubs without slipping and is pulled by the 100-N force applied to the cord wrapped around its outer rim. If the wheel starts from rest, compute its angular velocity  $\omega$  after its center has moved a distance of 3 m up the incline. The wheel has a mass of 40 kg with center of mass at O and has a centroidal radius of gyration of 150 mm. Determine the power input from the 100-N force at the end of the 3-m motion interval.

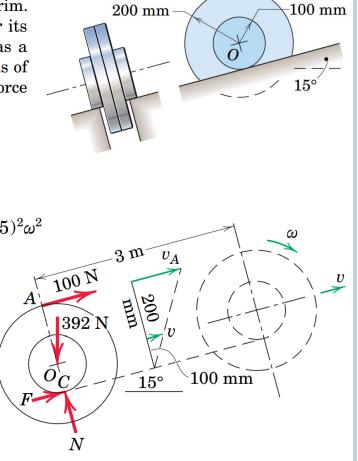
$$U_{1-2} = 100 \frac{200 + 100}{100} (3) - (392 \sin 15^{\circ})(3) = 595 \text{ J}$$

$$U_{1-2} = 100 \frac{100}{100} (3) - (392 \sin 13)(3) = 393 J$$
$$[T = \frac{1}{2}m\overline{v}^2 + \frac{1}{2}\overline{I}\omega^2] \qquad T_1 = 0 \qquad T_2 = \frac{1}{2}40(0.10\omega)^2 + \frac{1}{2}40(0.15)^2\omega^2$$
$$= 0.650\omega^2$$

$$[T = \frac{1}{2}I_C\omega^2] \qquad T = \frac{1}{2}40[(0.15)^2 + (0.10)^2]\omega^2 = 0.650\omega^2$$

$$[T_1 + U_{1-2} = T_2]$$
  $0 + 595 = 0.650\omega^2$   $\omega = 30.3 \text{ rad/s}$ 

$$P = \mathbf{F} \cdot \mathbf{v} ] \qquad P_{100} = 100(0.3)(30.3) = 908 \text{ W}$$





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100 N

### SECTION C Impulse and Momentum

<sup>6/8</sup> Impulse-Momentum Equations

#### Linear Momentum

$$\begin{array}{c} \mathbf{G} = m\overline{\mathbf{v}} \\ \hline \mathbf{G} = m\overline{\mathbf{v}} \\ \hline \mathbf{C}\mathbf{F} = \dot{\mathbf{G}} \\ \hline \mathbf{G}_1 + \int_{t_1}^{t_2} \Sigma \mathbf{F} \, dt = \mathbf{G}_2 \\ \hline \mathbf{G}_1 + \int_{t_1}^{t_2} \Sigma \mathbf{F} \, dt = (\mathbf{G}_x)_2 \\ \hline \mathbf{G}_x + \int_{t_1}^{t_2} \Sigma F_x \, dt = (\mathbf{G}_x)_2 \\ \hline \mathbf{G}_y + \int_{t_1}^{t_2} \Sigma F_y \, dt = (\mathbf{G}_y)_2 \end{array}$$



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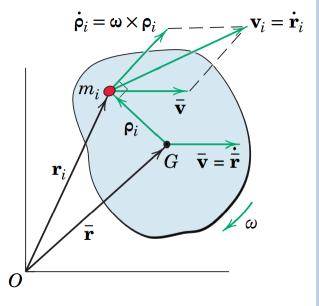
### <sup>6/8</sup> Impulse-Momentum Equations

### Angular Momentum

$$H_G = \overline{I}\omega$$

$$\Sigma M_G = \dot{H}_G$$

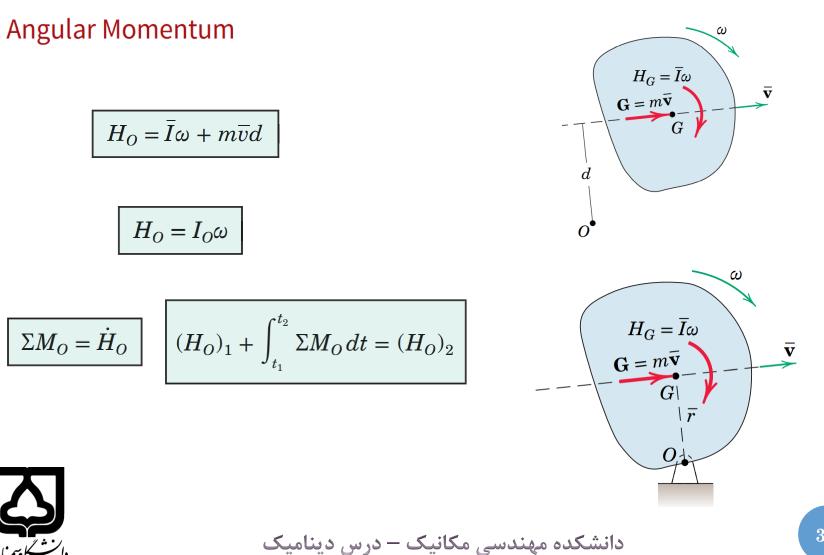
$$(H_G)_1 + \int_{t_1}^{t_2} \Sigma M_G dt = (H_G)_2$$





**Chapter 6 - Plane Kinetics of Rigid Bodies** 

### <sup>6/8</sup> Impulse-Momentum Equations



### <sup>6/8</sup> Impulse-Momentum Equations

**Conservation of Momentum** 

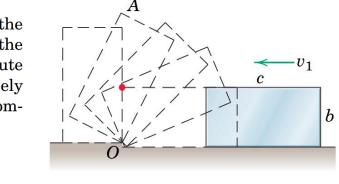
$$\mathbf{G}_1 = \mathbf{G}_2$$

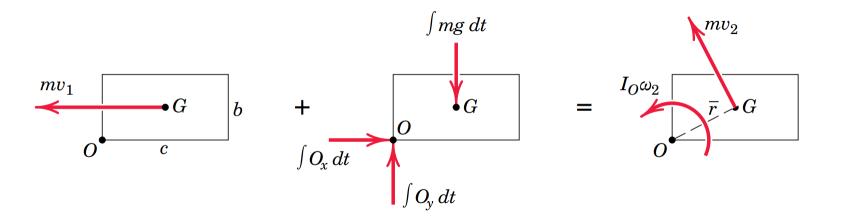
$$(\mathbf{H}_O)_1 = (\mathbf{H}_O)_2$$

$$(\mathbf{H}_G)_1 = (\mathbf{H}_G)_2$$



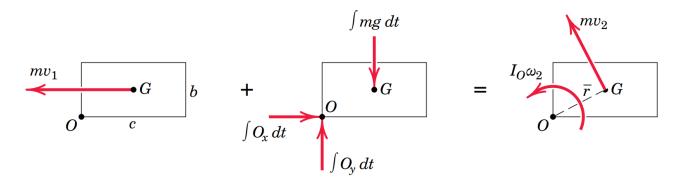
The uniform rectangular block of dimensions shown is sliding to the left on the horizontal surface with a velocity  $v_1$  when it strikes the small step at *O*. Assume negligible rebound at the step and compute the minimum value of  $v_1$  which will permit the block to pivot freely about *O* and just reach the standing position *A* with no velocity. Compute the percentage energy loss *n* for b = c.







Impact of Rigid Bodies

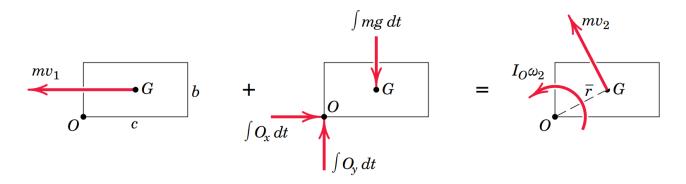


I. Collision

$$\begin{split} [H_0 = I_0 \omega] \qquad (H_0)_2 = \left\{ \frac{1}{12} m(b^2 + c^2) + m \left[ \left( \frac{c}{2} \right)^2 + \left( \frac{b}{2} \right)^2 \right] \right\} \omega_2 \\ = \frac{m}{3} (b^2 + c^2) \omega_2 \end{split}$$

$$[(H_O)_1 = (H_O)_2] \qquad mv_1 \frac{b}{2} = \frac{m}{3}(b^2 + c^2)\omega_2 \qquad \omega_2 = \frac{3v_1b}{2(b^2 + c^2)}$$





#### II. Rotation about O

$$\begin{split} [T_2 + V_2 &= T_3 + V_3] & \frac{1}{2} I_0 \omega_2^2 + 0 = 0 + mg \left[ \sqrt{\left(\frac{b}{2}\right)^2 + \left(\frac{c}{2}\right)^2 - \frac{b}{2}} \right] \\ & \frac{1}{2} \frac{m}{3} (b^2 + c^2) \left[ \frac{3v_1 b}{2(b^2 + c^2)} \right]^2 = \frac{mg}{2} \left( \sqrt{b^2 + c^2} - b \right) \\ & v_1 = 2 \sqrt{\frac{g}{3} \left(1 + \frac{c^2}{b^2}\right) \left( \sqrt{b^2 + c^2} - b \right)} \end{split}$$

$$n = \frac{|\Delta E|}{E} = \frac{\frac{1}{2}mv_1^2 - \frac{1}{2}I_0\omega_2^2}{\frac{1}{2}mv_1^2} = 1 - \frac{k_0^2\omega_2^2}{v_1^2} = 1 - \left(\frac{b^2 + c^2}{3}\right) \left[\frac{3b}{2(b^2 + c^2)}\right]^2$$
$$= 1 - \frac{3}{4\left(1 + \frac{c^2}{b^2}\right)} \qquad n = 62.5\% \text{ for } b = c$$

