



دانشگاه سمنان

Semnan University  
Faculty of Mechanical Engineering

دانشکده مهندسی مکانیک

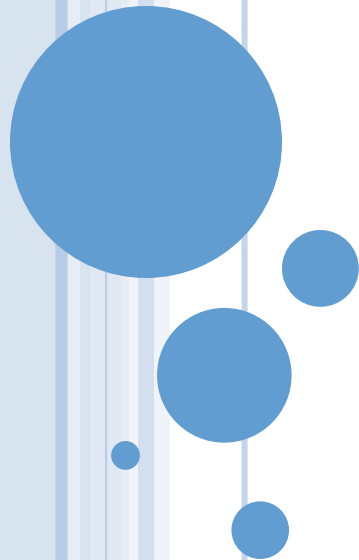


دانشکده مهندسی مکانیک

درس طراحی سیستم های شاسی  
خودرو

**VEHICLE CHASSIS  
SYSTEMS DESIGN**

*Chapter 3 – Braking Performance  
Class Lecture*



□ CONTENTS:

- ❖ Chapter 1: Introduction
- ❖ Chapter 2: Accelerating Performance
- ❖ Chapter 3: **Braking Performance**
- ❖ Chapter 4: Road Loads
- ❖ Chapter 5: Ride
- ❖ Chapter 6: Cornering
- ❖ Chapter 7: Suspension
- ❖ Chapter 8: Steering System
- ❖ Chapter 9: Roll-over

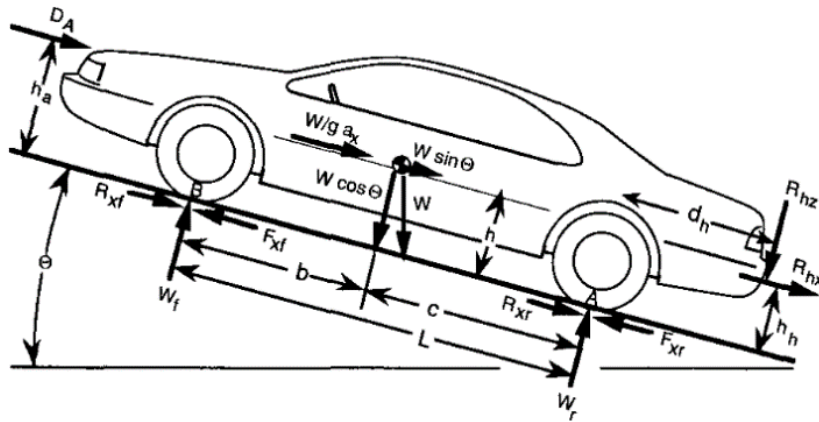


## BASIC EQUATIONS

□ The general equation for braking performance:

❖ Newton's Second Law for the x-direction

$$\longrightarrow M a_x = - \frac{W}{g} D_x = - F_{xf} - F_{xr} - D_A - W \sin \Theta$$



$W$  = Vehicle weight

$g$  = Gravitational acceleration

$D_x = - a_x$  = Linear deceleration

$F_{xf}$  = Front axle braking force

$F_{xr}$  = Rear axle braking force

$D_A$  = Aerodynamic drag

$\Theta$  = Uphill grade

## BASIC EQUATIONS

- Constant Deceleration:

$$\longrightarrow D_x = \frac{F_{xt}}{M} = - \frac{dV}{dt}$$

$F_{xt}$  = The total of all longitudinal deceleration forces on the vehicle (+)

$V$  = Forward velocity

- This equation can be integrated:

$$\longrightarrow \int_{V_o}^{V_f} dV = - \frac{F_{xt}}{M} \int_0^{t_s} dt \quad \longrightarrow \quad V_o - V_f = \frac{F_{xt}}{M} t_s$$



## BASIC EQUATIONS

- Relationship between velocity and distance:

$$\longrightarrow \frac{V_o^2 - V_f^2}{2} = \frac{F_{xt}}{M} X \quad X = \text{Distance traveled during the deceleration}$$

- Deceleration to full stop ( $V_f = 0$ ):

- ❖ X: Stopping Distance, SD

$$\longrightarrow SD = \frac{V_o^2}{2 \frac{F_{xt}}{M}} = \frac{V_o^2}{2 D_x}$$

- ❖  $t_s$ : Stopping Time

$$\longrightarrow t_s = \frac{V_o}{\frac{F_{xt}}{M}} = \frac{V_o}{D_x}$$



## BASIC EQUATIONS

### □ Deceleration with Wind Resistance:

- ❖ The aerodynamic drag on a vehicle is dependent on vehicle drag factors and the square of the speed.

$$\longrightarrow \sum F_x = F_b + C V^2$$

$F_b$  = Total brake force of front and rear wheels

$C$  = Aerodynamic drag factor

$$\longrightarrow \int_0^{SD} dx = M \int_{V_0}^0 \frac{V dV}{F_b + C V^2} \quad \longrightarrow SD = \frac{M}{2C} \ln \left[ \frac{F_b + C V_0^2}{F_b} \right]$$



## BASIC EQUATIONS

### □ Energy/Power:

- ❖ The energy and/or power absorbed by a brake system

$$\longrightarrow \text{Energy} = \frac{M}{2} (V_o^2 - V_f^2)$$

$$\longrightarrow \text{Power} = \frac{M}{2} \frac{V_o^2}{t_s}$$

## BRAKING FORCES

### □ Rolling Resistance:

- ❖ Rolling resistance always opposes vehicle motion

$$\longrightarrow R_{xf} + R_{xr} = f_r (W_f + W_r) = f_r W$$

- ❖ The parameter " $f_r$ " is the rolling resistance coefficient.
- ❖ The total force is independent of the distribution of loads on the axles (static or dynamic).
- ❖ Rolling resistance forces are nominally equivalent to about 0.01 g deceleration.





## BRAKING FORCES

### ❑ Aerodynamic Drag:

- ❖ The drag from air resistance is proportional to the square of the speed.
- ❖ At low speeds it is negligible.
- ❖ At normal highway speeds, it may contribute a force equivalent to about 0.03 g

### ❑ Driveline Drag:

- ❖ The engine, transmission, and final drive contribute both drag and inertia effects to the braking action.
- ❖ Whether or not driveline drag aids in braking depends on the rate of deceleration.



## BRAKING FORCES

### □ Grade:

- ❖ Road grade will contribute directly to the braking effort, either in a positive sense (uphill) or negative (downhill).

$$\longrightarrow R_g = W \sin \Theta \cong W \Theta$$

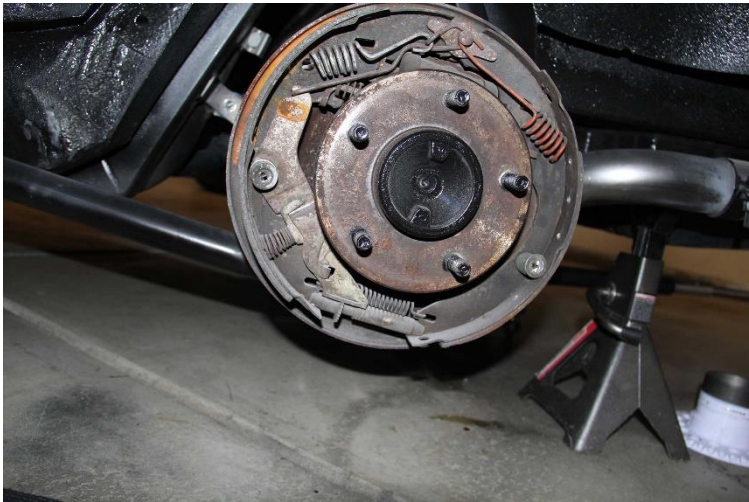
- ❖ A grade of 4% (0.04) will be equivalent to a deceleration of  $\pm 0.04 g$



## BRAKING FORCES

### □ BRAKES

- ❖ Automotive brakes in common usage today are of two types:
  - ✓ Drum Brake
  - ✓ Disc Brake



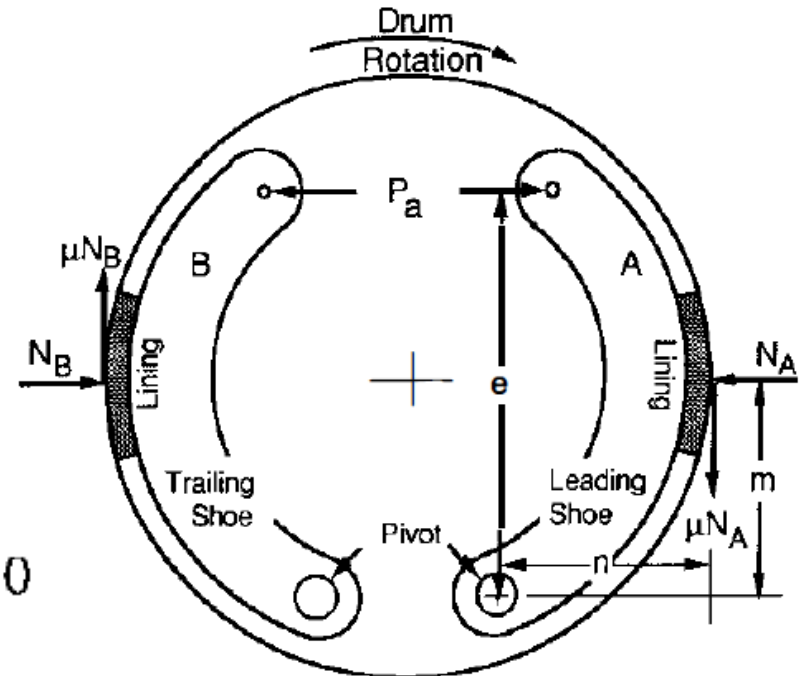
## BRAKING FORCES

### □ Brake Factor:

❖ Mechanical advantage that can be utilized in drum brakes to minimize the actuation effort required.

❖ Some of torques about P:

$$\rightarrow \Sigma M_p = e P_a + n \mu N_A - m N_A = 0$$



$e$  = Perpendicular distance from actuation force to pivot

$N_A$  = Normal force between lining A and drum

$n$  = Perpendicular distance from lining friction force to pivot

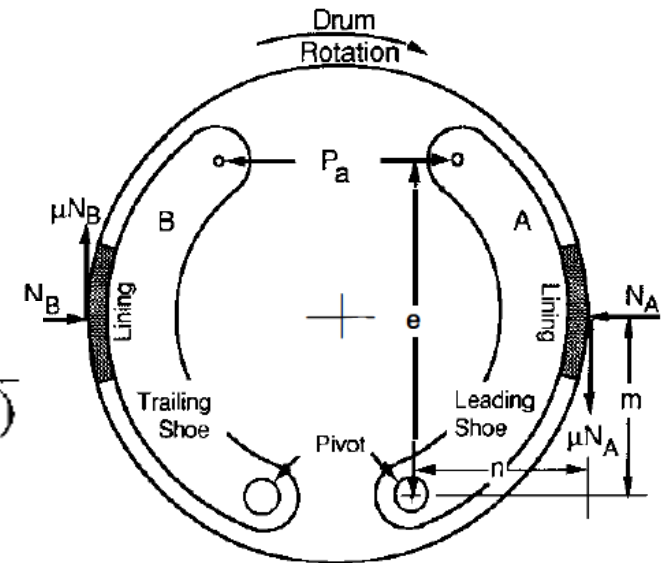
$m$  = Perpendicular distance from the normal force to the pivot

## BRAKING FORCES

- The friction force developed

$$\rightarrow F_A = \mu N_A \quad \text{and} \quad F_B = \mu N_B$$

$$\rightarrow \frac{F_A}{P_a} = \frac{\mu e}{(m - \mu n)} \quad \text{and} \quad \frac{F_B}{P_a} = \frac{\mu e}{(m + \mu n)}$$

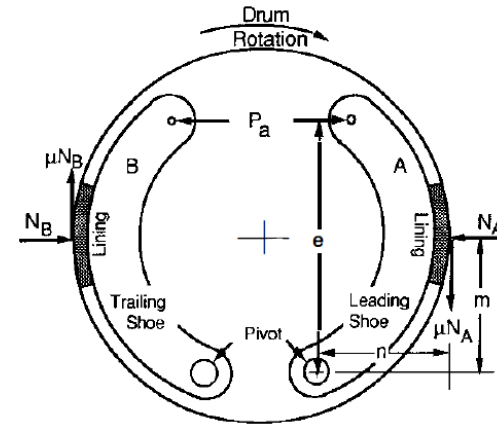


- ❖ The shoe on the right is a "leading" shoe.

## BRAKING FORCES

### □ The friction force developed

- ❖ The shoe on the right is a "leading" shoe.
- ❖ The moment produced by the friction force on the shoe acts to rotate it against the drum and increase the friction force developed.
- ❖ Shoe B is a trailing shoe configuration on which the friction force acts to reduce the application force.
- ❖ By using two leading shoes, two trailing shoes, or one of each, different brake factors can be obtained.



## BRAKING FORCES

- Brake torque performance can be measured in the laboratory using an inertial dynamometer.
- ❖ It can be difficult to predict accurately over all conditions

$$\longrightarrow T_b = f(P_a, \text{Velocity}, \text{Temperature})$$

$$\longrightarrow F_b = \frac{(T_b - I_w \alpha_w)}{r}$$

$r$  = Rolling radius of the tires

$I_w$  = Rotational inertia of wheels (and drive components)

$\alpha_w$  = Rotational deceleration of wheels

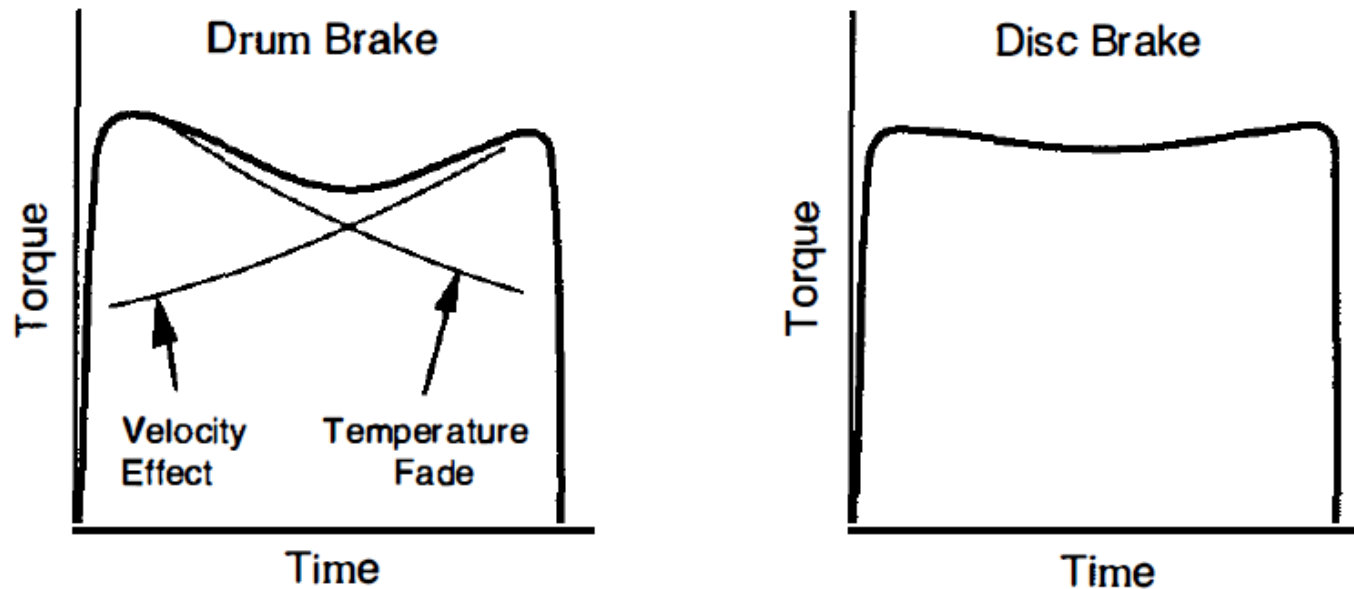
- ❖ Neglecting the wheels:

$$\longrightarrow F_b = \frac{T_b}{r}$$



## BRAKING FORCES

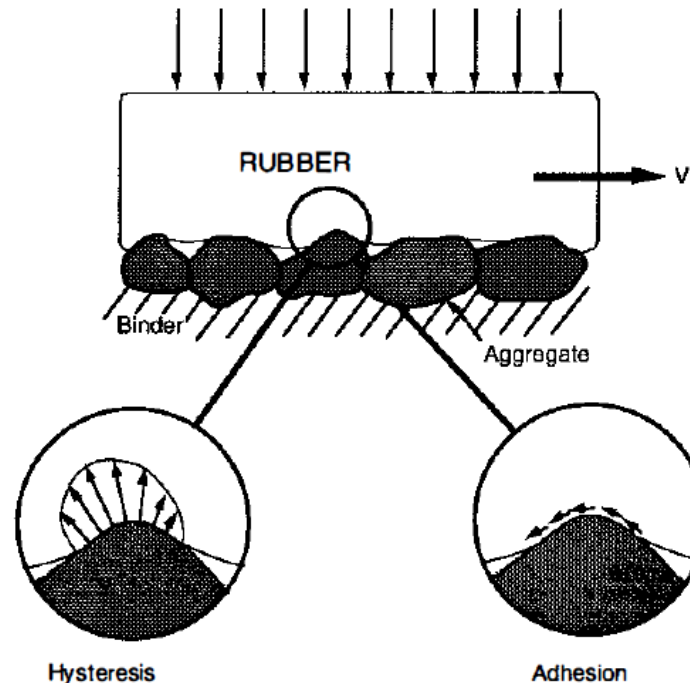
### □ Brake torque performance





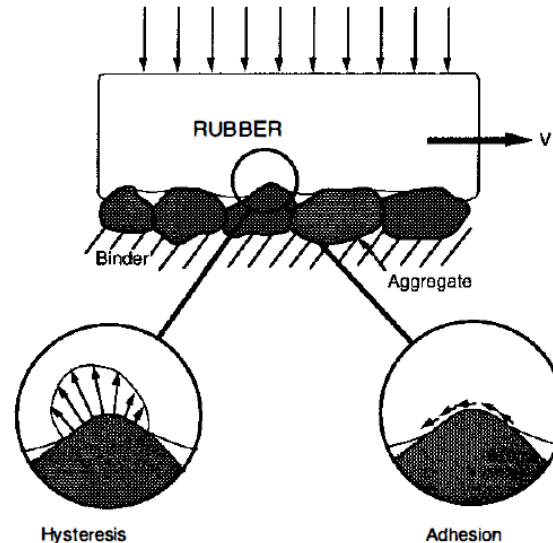
## TIRE-ROAD FRICTION

- The brake force limit: frictional coupling between the tire and road
  - ❖ There are two primary mechanisms
    - ✓ Surface adhesion (intermolecular bonds between the rubber and the road surface)
    - ✓ Hysteresis (energy loss in the rubber as it deforms when sliding)



## TIRE-ROAD FRICTION

- ❖ The adhesion component is the larger of the two mechanisms on dry roads, but is reduced substantially when the road surface is contaminated with water.
- ❖ Bulk (or hysteretic) friction is not so affected by water on the road surface, thus better wet traction is achieved with tires that have high-hysteresis rubber in the tread.



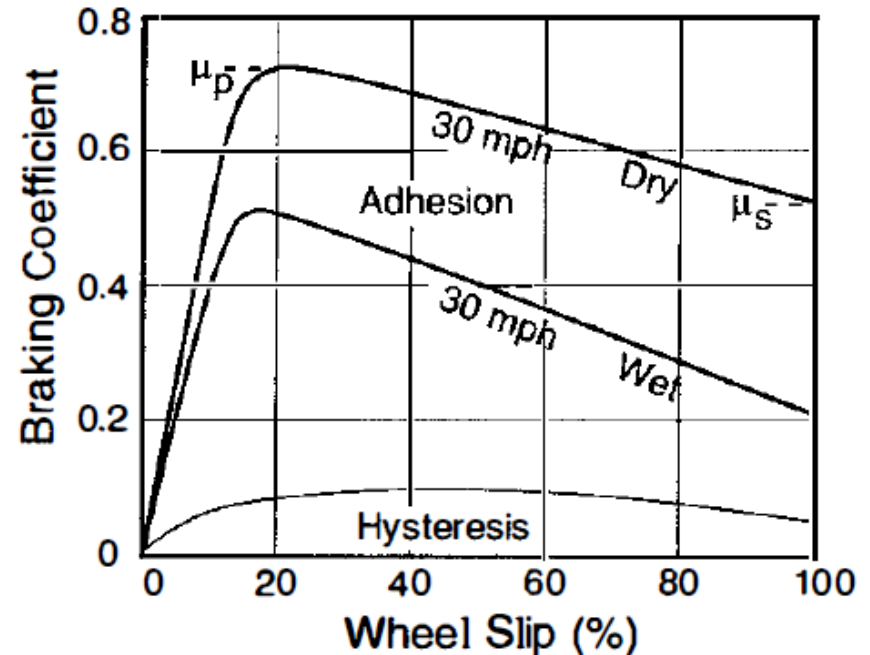
## TIRE-ROAD FRICTION

- Both adhesive and hysteretic friction depend on some small amount of slip occurring at the tire-road interface.

$$\rightarrow \text{Slip} = \frac{V - \omega r}{V}$$

$V$  = Vehicle forward velocity

$\omega$  = Tire rotational speed (radians/sec)



## TIRE-ROAD FRICTION

### ❑ Other Parameters:

#### ❖ Velocity

- ✓ On dry roads, both peak and slide friction decrease with velocity.
- ✓ Under wet conditions, even greater speed sensitivity prevails because of the difficulty of displacing water

#### ❖ Inflation Pressure

- ✓ On dry roads, peak and slide coefficients are only mildly affected by inflation pressure.
- ✓ On wet surfaces, inflation pressure increases are known to significantly improve both coefficients

#### ❖ Vertical Load

- ✓ Increasing vertical load is known to categorically reduce normalized traction levels ( $F_x/F_z$ ) under both wet and dry conditions.



## FEDERAL REQUIREMENTS FOR BRAKING PERFORMANCE

### □ Automotive Safety:

#### ❖ Federal Motor Vehicle Safety Standard (FMVSS)

#### ❖ FMVSS 105

- ✓ Establishing braking performance requirements for vehicles with hydraulic brake systems

#### ❖ FMVSS 121

- ✓ Establishing braking performance requirements for vehicles with air brake systems

## BRAKE PROPORTIONING

- ❑ Lockup reduces the brake force on an axle, and results in some loss of ability to control the vehicle.
- ❑ Preferred design is to bring both axles up to the lockup point simultaneously.

❑ For :  $W_f = \frac{c}{L} W + \frac{h}{L} \frac{W}{g} D_x = W_{fs} + W_d$

$$W_r = \frac{b}{L} W - \frac{h}{L} \frac{W}{g} D_x = W_{rs} - W_d$$

$W_{fs}$  = Front axle static load

$W_{rs}$  = Rear axle static load

$W_d = (h/L) (W/g) D_x$  = Dynamic load transfer

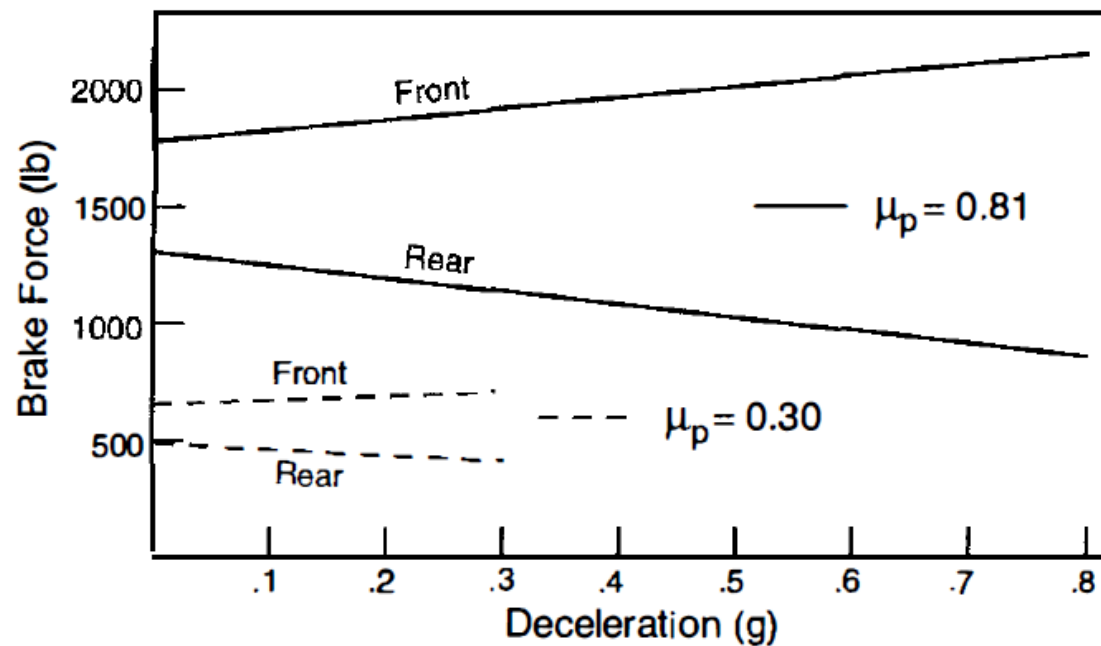


## BRAKE PROPORTIONING

- The maximum brake force on each axle:

$$F_{xmf} = \mu_p W_f = \mu_p \left( W_{fs} + \frac{h}{L} \frac{W}{g} D_x \right)$$

$$F_{xmr} = \mu_p W_r = \mu_p \left( W_{rs} - \frac{h}{L} \frac{W}{g} D_x \right) \quad \mu_p = \text{Peak coefficient of friction}$$



## BRAKE PROPORTIONING

- Also the deceleration is a function of the total braking force imposed on the vehicle

$$D_x = \frac{(F_{xmf} + F_{xp})}{M}$$

$$F_{xmf} = \frac{\mu_p (W_{fs} + \frac{h}{L} F_{xr})}{1 - \mu_p \frac{h}{L}}$$

$$D_x = \frac{(F_{xmr} + F_{xf})}{M}$$

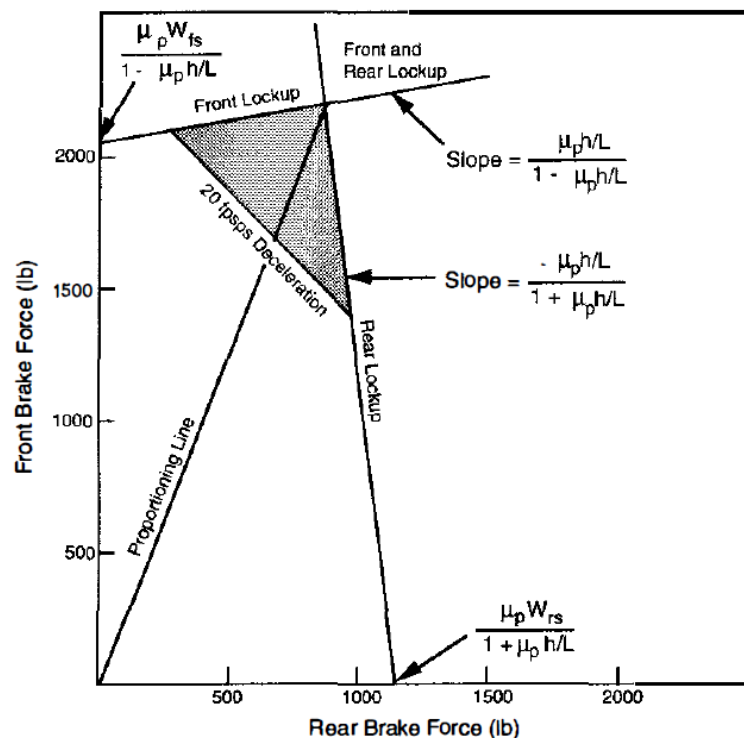
$$F_{xmr} = \frac{\mu_p (W_{rs} - \frac{h}{L} F_{xf})}{1 + \mu_p \frac{h}{L}}$$



## BRAKE PROPORTIONING

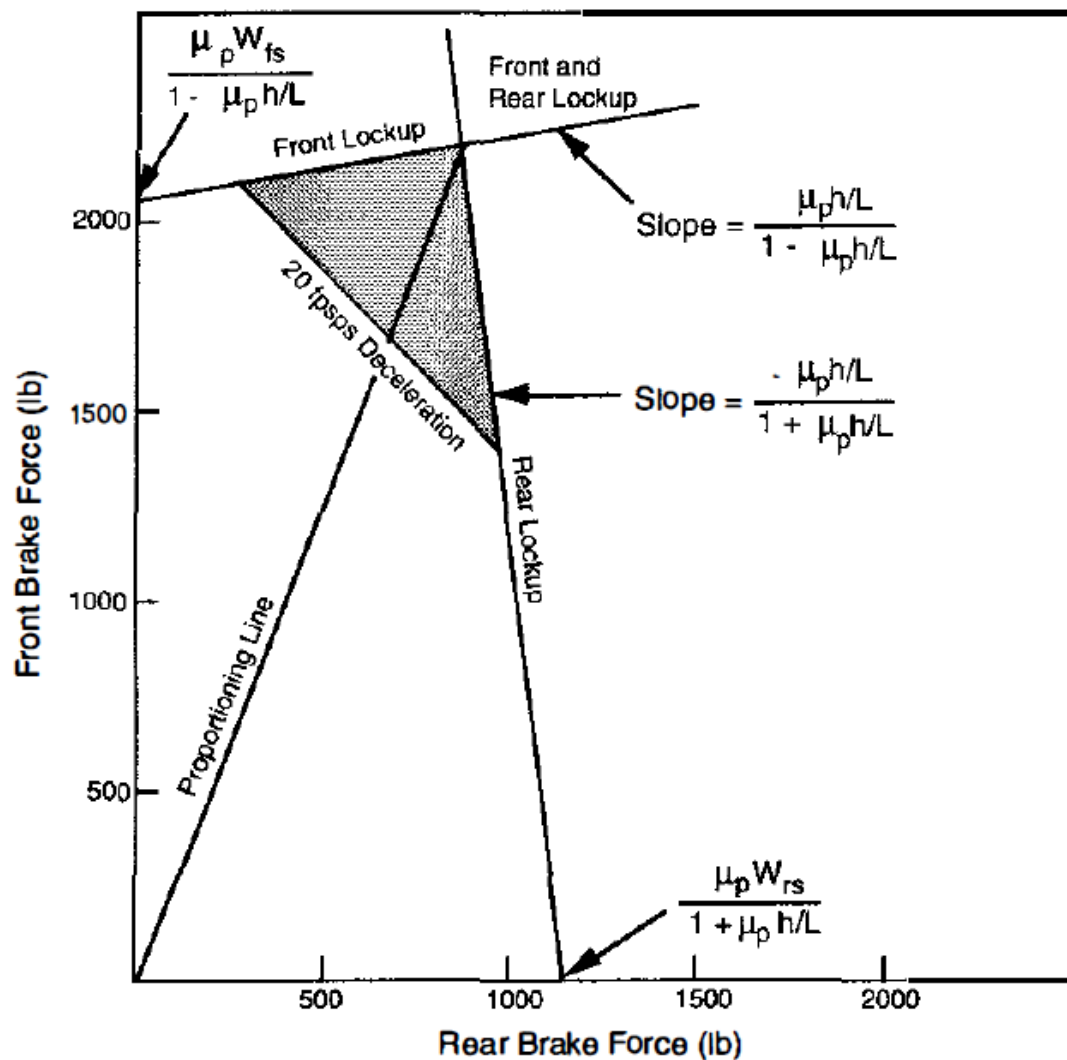
## □ "Brake proportioning"

- ❖ Relationship between front and rear brake forces determined by the pressure applied to each brake and the gain of each



## BRAKE PROPORTIONING

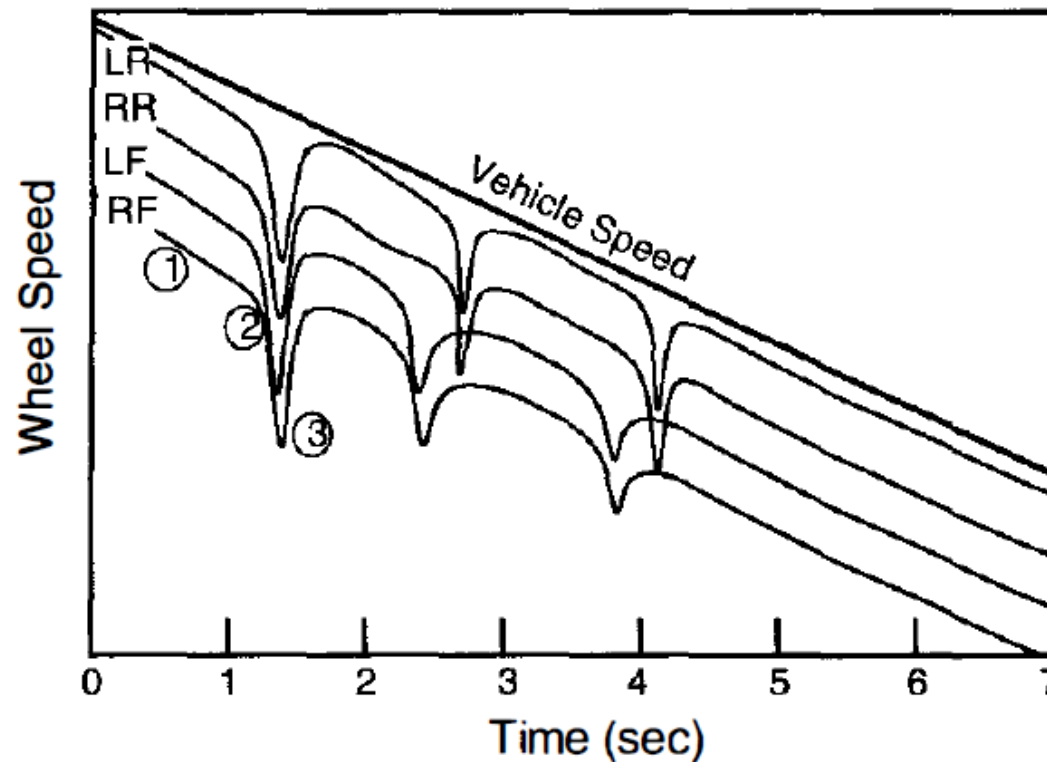
## □ "Brake proportioning"



## ANTI-LOCK BRAKE SYSTEMS

### ❑ Anti-lock systems (ABS):

- ❖ Sense when wheel lockup occurs, release the brakes momentarily on locked wheels, and reapply them when the wheel spins up again.



## BRAKING EFFICIENCY

### ❑ Braking efficiency, $\eta_b$ :

- ❖ Ratio of actual deceleration achieved to the "best" performance possible on the given road surface
- ❖ The best performance any vehicle can achieve is a braking deceleration (in g's) equivalent to coefficient of friction between the tires and the road surface

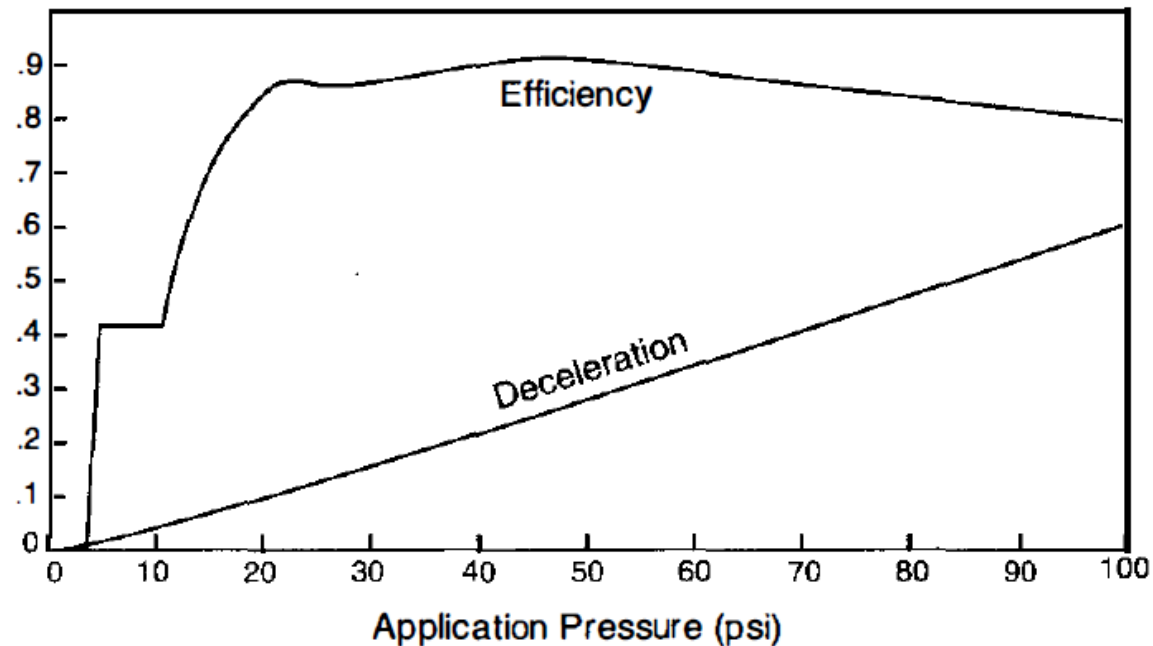
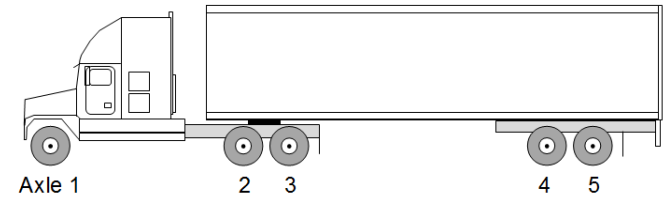
$$\eta_b = \frac{D_{act}}{\mu_p}$$

- ❖ Braking efficiency is a useful method for evaluating the performance of brake systems, especially on heavy trucks where multiple axles are involved.



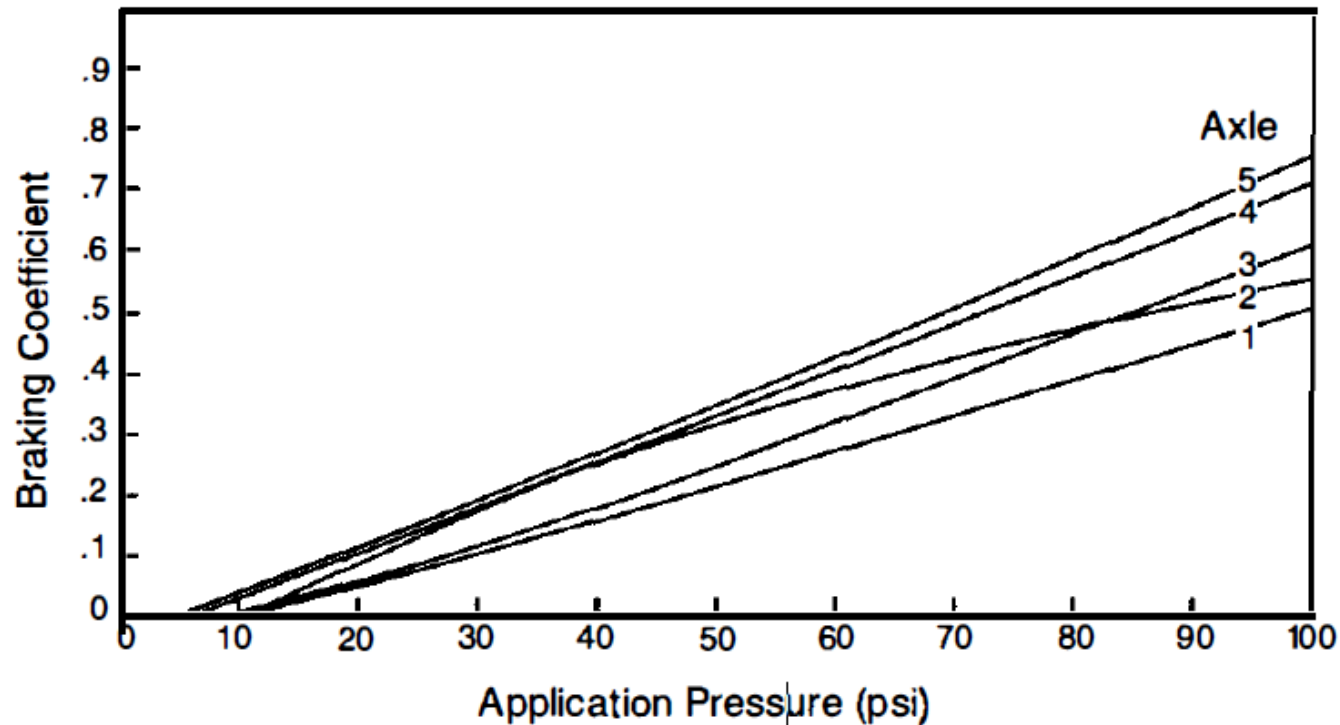
## BRAKING EFFICIENCY

- Braking efficiency calculated for a five-axle tractor semitrailer:



## BRAKING EFFICIENCY

- Contributions to braking from individual axles:



## PEDAL FORCE GAIN

### □ Ergonomics:

- ❖ The ease with which the driving public can optimally use the braking capabilities

